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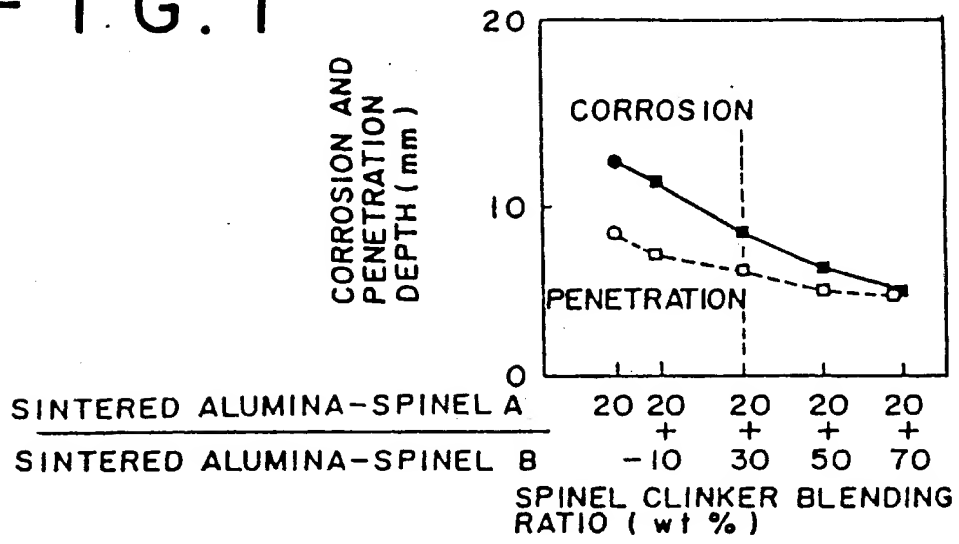
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**AT BE DE FR GB IT LU NL SE**(71) Applicant: **SHINAGAWA REFRACTORIES CO., LTD.**  
**2-1, Ohtemachi 2-chome Chiyoda-ku**  
**Tokyo 100(JP)**(72) Inventor: **YAMAMURA, Takashi, 700-121,**  
**Shinogoe**  
**Okayama-shi**  
**Okayama 703(JP)**  
Inventor: **HAMAZAKI, Yoshihisa, 8-21, Hamano**  
**4-chome**  
**Okayama-shi****Okayama 700(JP)**Inventor: **KANESHIGE, Toshihiko, 873 Inbe****Bizen-shi****Okayama 705(JP)**Inventor: **NANBA, Makoto, 390,****Higashikatakami****Bizen-shi****Okayama 705(JP)**Inventor: **KUBOTA, Yukitoshi, 16-24,****Sakuragaoka-nishi 7-chome Sanyocho****Akaiwa-gun****Okayama 709-08(JP)**(74) Representative: **Hansen, Bernd, Dr.**  
**Dipl.-Chem. et al**  
**Hoffmann, Eitle & Partner Patent- und**  
**Rechtsanwälte Arabellastrasse 4 Postfach**  
**81 04 20**  
**W-8000 München 81 (DE)**(54) **UNSHAPED ALUMINA SPINEL REFRACTORY.**

(57) An unshaped alumina spinel refractory excellent in spalling, corrosion and slag resistances, which comprises an alumina spinel clinker having a molar ratio of MgO to Al<sub>2</sub>O<sub>3</sub> of 0.14:1.86 to 0.6:1.4, optionally together with spinel clinker with an approximately theoretical composition based on the alumina spinel clinker, and the balance of sintered alumina and alumina cement. It is possible to suppress the extension of crack by adding crushed alumina particles with a particle size of 10 to 50 mm to the refractory.

FIG. 1



## Industrial Field of Use

This invention relates to alumina-spinel type monolithic refractories having excellent spalling resistance, corrosion resistance and slag penetration resistance.

## Prior Art

In recent years, the conditions for using lining refractories for ladles have become severe because of diversification of the steel making process, i.e. ① a rise in continuous casting ratio and an increase in degasification ratio; ② the introduction of ladle refining; and ③ a rise of tapping temperatures accompanying transportation of molten steel, extension of holding time of molten steel, agitation of molten steel and like.

In the past, lining refractories for ladles were based on Roseki and/or zircon refractories, but high-alumina refractories are now being used as refractories having a low silica content not only because of said diversification in the steel making process, but also because of strong demand for high quality steel. Also, even though basic materials such as magnesia refractories and the like were partially investigated, said materials never became practical, because of a great deal of cracking and peeling owing to thermal and structural spalling.

Compared with Roseki and zircon refractories, high-alumina refractories have the following disadvantages: (a) slag penetration is great, (b) spalling resistance is inferior.

As processes inhibiting slag penetration of high-alumina refractories, alumina-spinel type, alumina-spinel-magnesia type or alumina-magnesia type castable refractories that are combined with  $\text{MgO} \cdot \text{Al}_2\text{O}_3$  type spinel and/or magnesia were proposed in Japanese Patent Laid-Open Nos. 55-23004, 59-128271, 60-60985 and 64-87577.

In more detail, Japanese Patent Laid-Open No. 55-23004 described a material comprising from 10 to 85 percent by weight of a spinel clinker having a theoretical composition with a  $\text{MgO} \cdot \text{Al}_2\text{O}_3$  molar ratio of 1:1, from 5 to 30 percent by weight of an alumina and from 10 to 25 percent by weight of a high-alumina cement; Japanese Patent Laid-Open No. 59-128271 described a material comprising from 50 to 95 percent by weight of a spinel having an approximate theoretical composition with a  $\text{MgO} \cdot \text{Al}_2\text{O}_3$  molar ratio of from 0.8:1.2 to 1.1:0.9 and the balance being substantially  $\text{Al}_2\text{O}_3$ ; Japanese Patent Laid-Open No. 60-60985 described a material comprising at least 60 parts by weight of a spinel clinker having a theoretical composition, from 10 to 35 parts by weight of an alumina clinker and from 3 to 10 parts by weight of an alumina cement. Also, Japanese Patent Laid-Open No. 64-87577 described a material having good slag penetration resistance comprised of from 5 to 40 percent by weight of a spinel having an approximate theoretical composition with a  $\text{MgO} \cdot \text{Al}_2\text{O}_3$  molar ratio of from 0.7:1.3 to 1.3:0.7, from 50 to 90 percent by weight of an alumina clinker and from 3 to 25 percent by weight of an alumina cement.

## Problems the Invention Aims to Solve

However, although it was found that if spinel or magnesia is added to said materials, the structural spalling and corrosion resistance in said materials are improved by inhibiting slag penetration in comparison with conventional high-alumina refractories, their effect in regards to slag penetration is less than that of Roseki and zircon refractories.

For example when a conventional spinel clinker with a  $\text{MgO} \cdot \text{Al}_2\text{O}_3$  molar ratio close to the theoretical composition is used alone in an alumina-spinel type monolithic refractory as can be seen from the results shown in Fig.2 of the corrosion test of an alumina-spinel type monolithic refractory using sintered spinel A having an almost theoretical composition with a  $\text{MgO} \cdot \text{Al}_2\text{O}_3$  molar ratio of 1.02:0.98, there is a problem when the spinel clinker passes 40 percent in that it becomes easier for structural spalling to occur, because the slag penetration become large, even though corrosion resistance is increased.

Also, there have been various reports concerning the mechanism of inhibiting slag penetration and they describe that the effect of the addition of spinel clinker inhibits slag penetration by dissolving  $\text{FeO}$  and  $\text{MnO}$  components in the slag into the spinel clinker.

However, if the  $\text{FeO}$  and  $\text{MnO}$  components dissolve to produce a solid solution in the spinel, the lattice constant of the spinel increases, since the ionic radii of both  $\text{Fe}$  and  $\text{Mn}$  ions are greater than those of  $\text{Mg}$  ions and the slack in the texture occurs due to the expanding monolithic refractories. As the result, slag penetration was accelerated. Therefore in order to inhibit spinel slag penetration, alumina-spinel type monolithic refractories using alumina and spinel have been proposed, but at the present time, refractories having satisfactory properties have not yet been developed.

Accordingly, the development of the monolithic refractories having even lower slag penetration is desirable.

#### Means for Solving the Pertinent Problem

In view of said problem, the present inventors noticed the  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio of spinel clinker and carried out various experiments, as the result of which it was found that the slag penetration of alumina-spinel type monolithic refractories using spinel clinker having from 0.14:1.86 to 0.6:1.4 of  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio is notably lower than that of prior art monolithic refractories using alumina material and spinel clinker having larger than 0.6:1.4 of  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio, to complete the present invention.

The first embodiment of the alumina-spinel type monolithic refractory according to the present invention is characterized in that said refractory contains from 80 to 92 percent by weight of alumina-spinel type clinker having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio within 0.14:1.86 to 0.6:1.4 and from 8 to 20 percent by weight of alumina cement.

The second embodiment of the alumina-spinel type monolithic refractory according to the present invention is characterized in that said refractory contains from 5 to 92 percent by weight of alumina-spinel type clinker having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio within 0.14:1.86 to 0.6:1.4, not more than 87 percent by weight of alumina material and from 8 to 20 percent by weight of alumina cement.

The third embodiment of the alumina-spinel type monolithic refractory according to the present invention is characterized in that said refractory contains 100 parts by weight of the mixture comprising from 5 to 92 percent by weight of alumina-spinel type clinker having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio within 0.14:1.86 to 0.6:1.4, not more than 87 percent by weight of alumina material and from 8 to 20 percent by weight of alumina cement, and from 10 to 40 parts by weight of alumina crushed grain having a grain size of from 10 to 50 mm.

Further, as for alumina-spinel type monolithic refractories using only alumina-spinel type clinker having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio within 0.14:1.86 to 0.6:1.4 as described above, it is clear from the results of a corrosion test of the material using only alumina-spinel type clinker having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio of 0.44:1.56 as shown as one example in Fig.3 that although excellent slag penetration resistance is obtained by said refractories, it was found that there is a problem in that the corrosion resistance of said refractories is slightly inferior to that using  $\text{MgO}-\text{Al}_2\text{O}_3$  type spinel clinker having a theoretical composition.

Accordingly, we found that in order to improve the durability of alumina-spinel type monolithic refractories during more severe service conditions if an alumina-spinel type clinker having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio within from 0.14:1.86 to 0.6:1.4 as described above and conventional spinel clinker having a close to theoretical composition are used together and blended at proper grain size and proper quantity, the refractories obtained have excellent slag penetrating resistance and the corrosion resistance can be significantly improved.

Accordingly, the fourth embodiment of the alumina-spinel type monolithic refractory according to the present invention is characterized in that said refractory contains from 10 to 40 percent by weight of spinel clinker having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio within 0.9:1.1 to 1.3:0.7 and a grain size of not more than 1 mm, from 30 to 82 percent by weight of alumina-spinel clinker having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio within 0.14:1.86 to 0.6:1.4 and from 8 to 20 percent by weight of alumina cement.

Also, the fifth embodiment of the alumina-spinel type monolithic refractory according to the present invention is characterized in that said refractory contains from 10 to 40 percent by weight of spinel clinker having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio within 0.9:1.1 to 1.3:0.7 and a grain size of not more than 1 mm, from 30 to 82 percent by weight of alumina-spinel clinker having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio within 0.14:1.86 to 0.6:1.4, not more than 45 percent by weight of alumina material and from 8 to 20 percent by weight of alumina cement.

#### Brief Explanation of the Drawings

Fig.1 is a graphical representation of a blending ratio of spinel clinkers having different  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratios, and of the relation between corrosion resistance and slag penetration resistance.

Fig.2 is a graphical representation of a blending ratio (percent by weight) of sintered spinel A having a close to theoretical composition ( $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio of 1.02:0.98), and the corrosion resistance and the slag penetration resistance when said sintered spinel A is singly used that is with the balance being sintered alumina and alumina cement.

Fig.3 is a graphical representation of a blending ratio (percent by weight) of sintered alumina-spinel B having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio of 0.44:1.56, and of the corrosion resistance and the slag penetration

resistance when said sintered alumina-spinel B is singly used that is with the balance being sintered alumina and alumina cement.

#### Operation

The alumina-spinel type clinker used in alumina-spinel type monolithic refractory according to the present invention may be selected from one or more of electromelting spinel clinkers and sintered spinel clinkers, with said alumina-spinel type clinkers having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio within 0.14:1.86 to 0.6:1.4 that is dissolved alumina with spinel to produce a solid solution, but said clinkers may contain a small amount of corundum.

Accordingly, it is desired that the  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio of an alumina-spinel type clinker using the present invention having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio of less than the theoretical composition ( $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio of 1:1) be within the range of 0.14:1.86 to 0.6:1.4 as described above. If said  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio is less than 0.14:1.86, the slag penetration effect is poor, and if said  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio is more than 0.6:1.4, at the time of the immersion of FeO and MnO components in the slag to the monolithic refractory the expansion of the refractory is occurs by enlarging the lattice constant of spinel solid solution in said refractory, thereby increasing the slack in the texture and slag penetration of said refractory.

Also, since the coefficient of thermal expansion of the alumina-spinel type clinker using the present invention is lower than that of spinel clinker having a theoretical composition ( $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio is 1:1), the thermal spalling resistance of the present refractories is better than that of the refractories using the spinel clinker having theoretical composition alone.

In the first, the second and the third embodiments according to the present invention the blending amounts of said alumina-spinel type clinker range from 5 to 92 percent by weight. If said blending amount is less than 5 percent by weight, the effect of inhibiting the slag penetration of alumina-spinel clinker is small and if said amount is more than 92 percent by weight, the blending amount of alumina cement that is binder is lowered and then a drop in strength of the refractory may occur. Further, if alumina material is not added, the blending amount is preferably from 80 to 92 percent by weight in consideration of the blending amount of alumina cement as described hereinafter.

Also in the fourth and fifth embodiments according to the present invention the blending amounts of alumina-spinel type clinker range from 30 to 82 percents by weight. Namely, as can be understood from the graphical representation of the relationship of the blending amount, the corrosion resistance and the slag penetration resistance shown in Fig.1, if this blending amount is less than 30 percent by weight, a high degree of corrosion resistance can not be obtained and further, it is not preferable for the blending amount to be more than 82 percent by weight, because the blending amounts of the spinel clinker and alumina cement that are blended simultaneously can not be 10 percent and over and can not be 8 percent and over by weight respectively, and high degrees of corrosion resistance and strength can not be obtained.

In Fig.1 sintered spinel A has a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio of 1.02:0.98 and sintered alumina-spinel B has a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio of 0.44:1.56.

Next, the spinel clinker used in the fourth and fifth embodiments of the present invention may be either an electromelting spinel or sintered spinel or these spinels may be used together. The  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio of said spinel clinker ranges from 0.9:1.1 to 1.3:0.7 and the grain size that can be used is less than 1 mm. If this grain size is more than 1 mm, the excellent slag penetration resistance can not be obtained which is undesirable. Also, the blending amount of spinel clinker ranges from 10 to 40 percent by weight. It is not preferable for this blending amount to either be less than 10 percent by weight, because a high degree of corrosion resistance can not be obtained nor to be more than 40 percent by weight, because the slag penetration resistance is lowered.

Further, sintered alumina, electromelting alumina, bauxite and aluminous shale can be used as alumina materials in the present invention. However, since an increase of silica content may incur the formation of low melting point materials, the use of sintered alumina and/or electromelting alumina is desired. If bauxite and/or aluminous shale, etc. are added, they are preferably in the form of coarse grains (not less than 3 mm and not more than 10 mm).

Further, the blending amounts of alumina materials in the second and third embodiments according to the present invention, are less than 87 percent by weight. If this blending amount is more than 87 percent by weight, problems concerning slag penetrating and strength may occur since the blending amounts of spinel clinker and alumina cement are lowered.

Also, if alumina material is added in the fourth and fifth embodiments according to the present invention, the blending amount of said material is less than 45 percent by weight. That is it is not preferable that the blending amount be more than 45 percent by weight, because a high degree of corrosion resistance can

not be obtained.

Alumina cement has been used in conventional castable refractories and in the present invention alumina cement is used as binder. It is preferable that the blending amount of alumina cement range from 8 to 20 percent by weight. If this blending amount is less than 8 percent by weight, the strength of the refractory is insufficient and if this amount is more than 20 percent by weight, a large amount of low melting point material is formed and corrosion resistance is lowered.

In the third embodiment of the present invention, in order to inhibit the enlargement of cracks, alumina crushed grain such as electromelting alumina, aluminous shale, alumina brick and the like having a grain size of from 10 to 50 mm can be added in a blending amount of from 10 to 40 percent by weight of the total amount of the above materials such as alumina-spinel type clinker, alumina cement and spinel clinker.

Also, in alumina-spinel type monolithic refractories according to the present invention inorganic fibers, steel fibers, setting adjunct and like can be added.

Further, as processes for applying the alumina-spinel type monolithic refractories according to the present invention, casting processes, spray gunning processes and like can be used.

### Examples

In order to exemplify the alumina-spinel type monolithic refractories according to the present invention, the following examples are provided.

#### Example 1

In this Example, alumina-spinel type monolithic refractories related to the first, to the second and to the third embodiments are described. In Table 1, the chemical compositions of the materials used in the Working Examples and Comparative Examples are described and in Table 2, the blending ratios and properties of the monolithic refractories of the Working Examples and Comparative Examples are indicated.

Table 1

Component	SiO <sub>2</sub>	Al <sub>2</sub> O <sub>3</sub>	Fe <sub>2</sub> O <sub>3</sub>	TiO <sub>2</sub>	CaO	MgO	MgO:Al <sub>2</sub> O <sub>3</sub> molar ratio
Material							
Sintered Alumina	0.1	99.3	0.1	trace	0.1	0.1	
Sintered Alumina-Spinel A	0.1	94.3	0.2	trace	0.3	5.2	0.24:1.76
Sintered Alumina-Spinel B	0.1	89.4	0.2	trace	0.3	10.1	0.44:1.56
Sintered Spinel C	0.2	70.3	0.4	trace	0.3	28.9	1.02:0.98
Electromelting Alumina-Spinel A	0.4	82.6	1.0	0.1	0.8	14.3	0.61:1.39
Aluminous Shale	5.9	87.4	1.0	4.2	0.2	0.6	
Electromelting Alumina Crushed Grain	1.0	94.9	0.8	3.2	0.3	0.6	
Alumina Cement	0.2	79.8	0.3	trace	17.5	0.4	

Each compound indicated in Table 2 was mixed with a prescribed quantity of water, then cast and formed in a metallic frame, cured for 24 hours at 20 °C, and dried for 24 hours at 105 °C, and thereafter the obtained refractories were tested as follows:

(1) Linear Change After Heating (at 1500 °C -3 hours): according to JIS R2555.

(2) Corrosion Test

① Equipment: Rotary drum corrosion test equipment

② Sample size: 50 × 200 × 65 mm

③ Temperature and Time:

1650 °C - 30 minutes charging the slag

15 minutes! | 20 minutes 3 cycles

800 °C

|

1650 °C - 30 minutes heating

15 minutes! | 20 minutes 3 cycles

800 °C

④ Slag: LD Converter slag ( $\text{CaO/SiO}_2 = 3.65$ ) 1.2 kg/cycle

Table 2

Blending Amount(%)	Working Example												Comparative Example		
	1	2	3	4	5	6	7	8	9	10	1	2	3		
Sintered Alumina (5~1 mm)		50		40	40			50	50	40	50	50			
Sintered Alumina (not more than 1 mm)	18	25	8	8	20			18	18	8	18	35	14		
Sintered Alumina-Spinel A (5~1 mm)	50														
Sintered Alumina-Spinel A (not more than 1 mm)	20												50		
Sintered Alumina-Spinel B (5~1 mm)			50			50	50								
Sintered Alumina-Spinel B (not more than 1 mm)		10	30	30		38	38	20	20	30			30		
Sintered Spinel C (not more than 1 mm)											20				
Electromelting Alumina-Spinel A (5~1 mm)					10										
Electromelting Alumina-Spinel A (not more than 1 mm)					20							3			
Aluminous Shale (5~1 mm)				10						10					
Alumina Cement	12	15	12	12	10	12	12	12	12	12	12	12	6		
Electromelting Alumina Crushed grain (20~30 mm)	+20	+30	+25	+20		+25			+30		+20	+20	+20		
Added Water	5.0	5.0	5.0	5.5	6.5	5.0	6.0	6.0	5.0	6.5	5.0	5.0	5.0		
Linear Change(%)at 1500℃-3 hours	+0.03	0.00	-0.03	0.00	-0.03	-0.03	-0.03	+0.03	0.00	-0.03	+0.03	0.00	0.00		
Index of Corrosion Depth	125	120	105	130	90	100	100	120	110	135	100	130	80		
Index of slag Penetration Depth	60	55	45	65	55	50	45	50	55	60	100	155	140		
Spalling Resistance(*)	◎	◎	◎	◎	◎	◎	◎	◎	◎	◎	△	◎	△		
Test Result															

Spalling Test(\*): Test Method = Panel Spalling Method; Sample Size = 65 × 114 × 230 mm

Temperature and Time = Heating 1500°C - 30 min. ←→ Standing and Cooling 30 min. × 10 cycles.

◎ = a small number of cracks, ○ = a number of cracks, △ = a great number of cracks

# Example 2

In this Example, alumina-spinel type monolithic refractories related to the fourth and to the fifth embodiments are described. In Table 3, the chemical compositions of the materials used in the Working



Examples and Comparative Examples are described and in Table 4, the blending ratio and properties of the monolithic refractories of the Working Examples and Comparative Examples are indicated.

Table 3

Component	SiO <sub>2</sub>	Al <sub>2</sub> O <sub>3</sub>	Fe <sub>2</sub> O <sub>3</sub>	CaO	MgO	MgO:Al <sub>2</sub> O <sub>3</sub> molar ratio
Material						
Sintered Alumina	0.1	99.3	0.1	0.1	0.1	
Electromelting Alumina	0.1	99.5	0.1	0.1	0.1	
Sintered Spinel D	0.2	70.5	0.2	0.3	28.9	1.02:0.98
Sintered Alumina-Spinel B	0.1	89.4	0.2	0.3	10.1	0.44:1.56
Electromelting Alumina-Spinel E	0.4	82.6	0.2	0.8	14.3	0.60:1.40
Alumina Cement	0.2	79.8	0.2	17.7	0.4	

Each compound indicated in Table 4 was mixed with a prescribed quantity of water, then cast and formed in a metallic frame, cured for 24 hours at 20 °C, and dried for 24 hours at 105 °C, and thereafter the obtained refractories were tested as follows:

#### Corrosion Test

- ① Equipment: Rotary drum corrosion test equipment
- ② Sample size: 50 × 200 × 65 mm
- ③ Temperature and Time: 1650 °C - 4 hours
- ④ Slag: LD Converter slag

Table 4

	Blending Amount(%)	Working Example								Comparative Example							
		11	12	13	14	15	16	17		1	2	3	4	5	6	7	8
Sintered Alumina		40	20			20	20			10	40				70	40	10
Electromelting Alumina								20									
Sintered Spinel D (not more than 1 mm)		20	20	20	10	40	20	20			40				20		40
Sintered Spinel D (5~1 mm)										20	10						40
Sintered Alumina-Spinel B		30	50	70	80	30		50		30						50	80
Electromelting Alumina-Spinel E							50										
Alumina Cement		10	10	10	10	10	10	10		10	10	10	10	10	10	10	10
Corrosion Test Result Corrosion Depth (mm)		8	6	4.5	6	5	5	5.5		11	4.5				12	10.5	9
Penetration Depth (mm)		6	5	4.5	4	8	6	5.5		9	14				8	4	3

## Advantageous Effect of the Invention

The alumina-spinel type monolithic refractories according to the first, to the second and to the third embodiments of the present invention have good spalling resistance by inhibiting slag penetration in comparison with conventional alumina-spinel type monolithic refractories, because the MgO content in the

spinel material is selected.

Also, the alumina-spinel type monolithic refractories according to the fourth and the fifth embodiments of the present invention have both good slag penetration resistance and corrosion resistance, whereby durability can be significantly improved in lining refractories for ladles and like that are used under more severe service conditions and an excellent effect in the decrease of the cost of refractory can be obtained.

As described above, according to the alumina-spinel type monolithic refractories of the present invention, a monolithic refractory having less cracking and spalling can be provided, which is a material that can obtain stabilized high durability.

## Claims

1. An alumina-spinel type monolithic refractory characterized in that said refractory contains from 80 to 92 percent by weight of an alumina-spinel type clinker having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio ranging from 0.14:1.86 to 0.6:1.4 and includes from 8 to 20 percent by weight alumina cement.
2. An alumina-spinel type monolithic refractory characterized in that said refractory contains from 5 to 92 percent by weight of an alumina-spinel type clinker having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio ranging from 0.14:1.86 to 0.6:1.4, not more than 87 percent by weight alumina material and includes from 8 to 20 percent by weight alumina cement.
3. An alumina-spinel type monolithic refractory characterized in that said refractory contains a mixture 100 parts by weight which comprises 5 to 92 percent by weight of an alumina-spinel type clinker having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio ranging from 0.14:1.86 to 0.6:1.4, not more than 87 percent by weight alumina material and from 8 to 20 percent by weight alumina cement, and from 10 to 40 parts by weight alumina crushed grain having a grain size of 10 to 50 mm.
4. An alumina-spinel type monolithic refractory characterized in that said refractory contains from 10 to 40 percent by weight spinel clinker having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio ranging from 0.9:1.1 to 1.3:0.7 and a grain size of not more than 1 mm, from 30 to 82 percent by weight of an alumina-spinel clinker type clinker having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio ranging from 0.14:1.86 to 0.6:1.4 and from 8 to 20 percent by weight alumina cement.
5. An alumina-spinel type monolithic refractory characterized in that said refractory contains from 10 to 40 percent by weight spinel clinker having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio ranging from 0.9:1.1 to 1.3:0.7 and a grain size of not more than 1 mm, from 30 to 82 percent by weight of an alumina-spinel type clinker having a  $\text{MgO}:\text{Al}_2\text{O}_3$  molar ratio ranging from 0.14:1.86 to 0.6:1.4, not more than 45 percent by weight alumina material and from 8 to 20 percent by weight alumina cement.

FIG. 1

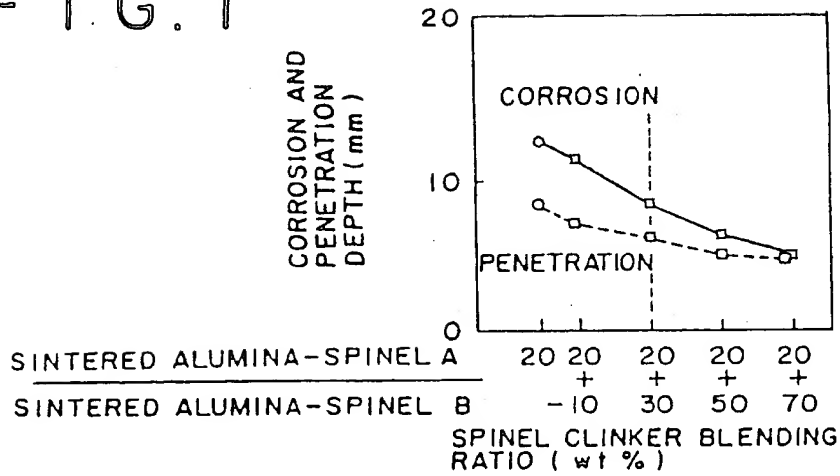


FIG. 2

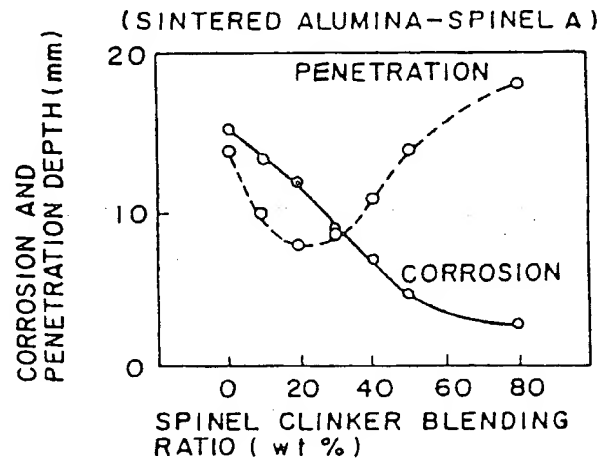
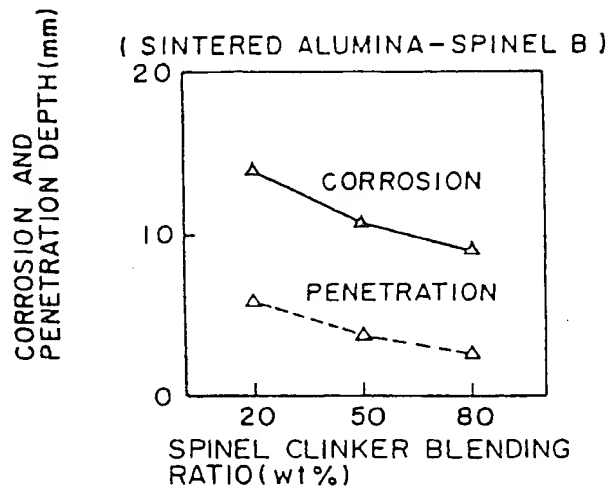


FIG. 3



# INTERNATIONAL SEARCH REPORT

International Application No PCT/JP91/01528

<b>I. CLASSIFICATION OF SUBJECT MATTER</b> (if several classification symbols apply, indicate all) *		
According to International Patent Classification (IPC) or to both National Classification and IPC		
Int. Cl <sup>5</sup> C04B35/66		
<b>II. FIELDS SEARCHED</b>		
Minimum Documentation Searched *		
Classification System	Classification Symbols	
IPC	C04B35/66	
Documentation Searched other than Minimum Documentation to the Extent that such Documents are Included in the Fields Searched *		
<b>III. DOCUMENTS CONSIDERED TO BE RELEVANT *</b>		
Category *	Citation of Document, ** with Indication, where appropriate, of the relevant passages **	Relevant to Claim No. **
X	JP, A, 60-60985 (Nippon Steel Corp.), April 8, 1985 (08. 04. 85), Line 12, lower right column, page 2 to lower column, page 3 (Family: none)	2, 3
Y	JP, A, 2-221165 (Harima Ceramic K.K.), September 4, 1990 (04. 09. 90), Line 10, upper left column to line 10, lower right column, page 2, Table 1 (Family: none)	1
Y	JP, A, 52-6713 (Kyushu Taika Renga K.K.), January 19, 1977 (19. 01. 77), Line 5, upper right column to line 7, lower right column, page 2 (Family: none)	1
<p>* Special categories of cited documents: **</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance: the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>"Y" document of particular relevance: the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art</p> <p>"&amp;" document member of the same patent family</p>		
<b>IV. CERTIFICATION</b>		
Date of the Actual Completion of the International Search	Date of Mailing of this International Search Report	
December 9, 1991 (09. 12. 91)	December 24, 1991 (24. 12. 91)	
International Searching Authority	Signature of Authorized Officer	
Japanese Patent Office		

